



Different Types of Synchronization Between Different Fractional Order Chaotic Systems

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Abstract: In this paper complete synchronization, anti-synchronization and projective synchronization are achieved between two different fractional order chaotic systems, fractional order Lotka Volterra system and fractional order Lu system, via active control method. Numerical simulations have been done in Matlab by using Grunwald Letnikov method. Numerical results demonstrate the effectiveness and feasibility of the proposed control techniques.

Keywords: *synchronization; anti-synchronization; projective synchronization; fractional order chaotic systems; active control*

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1 Introduction

A chaotic dynamical system is defined as the system which satisfies the properties of boundedness, infinite recurrence and sensitive dependence on initial conditions [2]. Chaos theory investigates the unstable behavior in deterministic nonlinear dynamical systems which cause 'chaos'. Sometimes chaotic behavior of a dynamical system is found useful like in secure communications [21, 37]. First time in 1963, Lorenz discovered a three dimensional chaotic system while studying weather model for atmospheric convection. After a decade, Rossler discovered a three dimensional chaotic system, which was constructed during the study of a chemical reaction. Synchronization is an important and famous phenomenon which can be understood within the unifying framework of the non-linear sciences. Due to its potential applications in the field of nonlinear dynamics it has been hot topic of research. Since the pioneer work of Pecora and Carroll [26] it has been

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an active area for researchers in applied sciences. Synchronization in the language of the nonlinear dynamics is defined as an adjustment of rhythms of oscillating objects due to their weak interaction. So many types of synchronization have been achieved: generalized synchronization [3], phase synchronization and anti-phase synchronization [4, 9, 34], lag synchronization [5], Q-S synchronization [24], etc. So many techniques have been developed for synchronization like adaptive control [14], feedback control [22], fuzzy control [7], nonlinear control [25], active backstepping [23], adaptive sliding mode control [38] etc. Chaos synchronization has so many applications in different fields like power systems [18], physics [39], chemistry [19], medicine [20], diffusion [12] etc.

Recently, fractional differential equations have been used to study different dynamical systems and chaos have been analyzed in different fractional order systems. So many numerical methods have been developed for the solution of fractional differential equation [29–31]. Also, fractional calculus is a 300 years old subject which can be traced back to Leibniz, Riemann, Grunwald and Letnikov. So many systems have been found in real life which can be represented more accurately by fractional order systems. But for the last few decades fractional calculus with chaos has been an attractive field and so many works have been done on synchronization and control of chaos in fractional order systems like Lorenz system [10], Rossler system [17], Volta System [28], Chua system [11], Chen system [16] etc. Recently so many new chaotic and hyperchaotic systems [8, 27, 32, 33, 35] have also been developed and analyzed by the researchers.

Synchronization has so many applications in which secure communication is very important. Synchronization between integer order and fractional order system via tracking control [13] and sliding mode control [6], synchronization of fractional order systems with different dimensions [36] and hybrid projective synchronization [15] of fractional order chaotic systems between order (1,2) have also been obtained in recent years. The aim of this paper is to achieve different synchronizations between different fractional order systems which is important for secure communication. Amongst different types of chaos synchronization, projective synchronization has been found to be more secure because of its unpredictable scaling factor and this is why it has received so much attention in the last few years.

In this paper we achieve three types of synchronization between two chaotic systems, fractional order Lotka Volterra system (master system) and fractional order Lu system (slave system) via active control. The achieved synchronizations are complete synchronization, anti-synchronization and projective synchronization. For numerical simulations Matlab software has been used and to solve fractional differential equation Grunwald Letnikov method has been used.

2 Fractional Order Derivatives [29]

Fractional calculus generalizes differentiation and integration to non integer order fundamental operator ${}_a D_t^\alpha$ where a and t are the limits of the operator and α is the non integer order. This operator is defined as

$${}_a D_t^\alpha = \begin{cases} \frac{d^\alpha}{dt^\alpha}, & : \alpha > 0 \\ 0, & : \alpha = 0 \\ \int_a^t (d\tau)^\alpha, & : \alpha < 0. \end{cases}$$

The most known three definitions for fractional integro differential operator are Riemann-Liouville definition, Grunwald-Letnikov definition and Caputo’s definition.

The Riemann-Liouville definition is given as

$${}_a D_t^\alpha f(t) = \frac{1}{\Gamma(n - \alpha)} \frac{d^n}{dt^n} \int_a^t (t - \tau)^{n-\alpha-1} f(\tau) d\tau, \quad n - 1 < \alpha < n.$$

The Caputo’s fractional derivative is defined as

$${}_0 D_t^\alpha = \frac{1}{\Gamma(n - \alpha)} \int_a^t \frac{f^n(\tau)}{(t - \tau)^{\alpha+1-n}} d\tau, \quad : n - 1 < \alpha < n,$$

where $\Gamma(\cdot)$ is the Gamma function, and the Grunwald Letnikov definition is

$${}_a D_t^\alpha f(t) = \lim_{h \rightarrow 0} \frac{1}{h^\alpha} \sum_{j=0}^{\lfloor \frac{t-\alpha}{h} \rfloor} (-1)^j \binom{\alpha}{j} f(t - jh),$$

where $\lfloor \cdot \rfloor$ denotes the greatest integer part.

3 Stability of Fractional Order System [13]

Theorem: *We consider the following linear fractional order system*

$$D^\alpha x = Ax, \quad x(0) = x_0. \tag{1}$$

Here, $A \in R^{n \times n}$, and $\alpha = (\alpha_1, \alpha_2, \dots, \alpha_n)$, $(0 < \alpha_i \leq 1)$. System (1) is asymptotically stable if and only if $|\arg(\lambda_i)| > \alpha\pi/2$ is satisfied for all eigenvalues λ_i of the matrix A . Furthermore, this system is stable if and only if $|\arg(\lambda_i)| \geq \alpha\pi/2$ is satisfied for all eigenvalues λ_i of the matrix A and those critical eigenvalues that satisfy the condition $|\arg(\lambda_i)| = \alpha\pi/2$ and have geometric multiplicity one. The geometric multiplicity of an eigenvalue is defined as the dimension of the associated eigenspace, i.e., the number of linearly independent eigenvectors with that eigenvalue.

Master and Slave systems. The fractional order Lotka-Volterra system [1] is considered as master system

$$\begin{aligned} \frac{d^{q_1} x_1}{dt^{q_1}} &= ax_1 - bx_1y_1 + ex_1^2 - sz_1x_1^2, \\ \frac{d^{q_2} y_1}{dt^{q_2}} &= dx_1y_1 - cy_1, \\ \frac{d^{q_3} z_1}{dt^{q_3}} &= sz_1x_1^2 - pz_1. \end{aligned} \tag{2}$$

This system exhibits chaotic behavior for parameter values $a = b = c = d = 1, e = 2, p = 3, s = 2.7$ and order $q_1 = q_2 = q_3 = 0.95$ for these values behavior of the system (2) is shown in Figure 1. Consider the following fractional order Lu chaotic system [29] as slave system

$$\begin{aligned} \frac{d^{q_1} x_2}{dt^{q_1}} &= \alpha(y_2 - x_2), \\ \frac{d^{q_2} y_2}{dt^{q_2}} &= \gamma y_2 - x_2 z_2, \\ \frac{d^{q_3} z_2}{dt^{q_3}} &= x_2 y_2 - \beta z_2, \end{aligned} \tag{3}$$

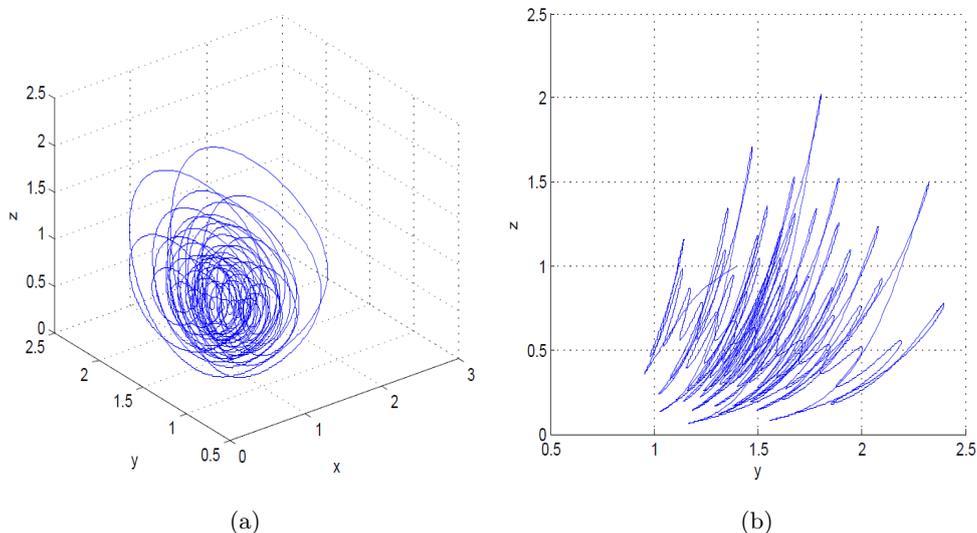


Figure 1: (a) Chaotic attractor of Lotka Volterra system in $x - y - z$ space for order $\alpha = 0.95$. (b) $y - z$ view of the Lotka-Volterra system for order $\alpha = 0.95$.

which exhibits chaotic behavior for parameters $\alpha = 36, \beta = 3, \gamma = 20$, and order $q_1 = q_2 = q_3 = 0.95$, as shown in Figure 2.

4 Synchronization Methodology and Numerical Simulations

To achieve different synchronizations between the considered two chaotic systems via active control method the error is defined as $e = y - \chi x$. For complete synchronization we take $\chi = 1$, for anti-synchronization $\chi = -1$, for projective synchronization arbitrary value of χ may be chosen. In this paper we took $\chi = 2$. Our aim is to design an effective controller $u(t)$ so that error e converges to zero. The master system is described by

$$\begin{aligned} \frac{d^{q_1} x_1}{dt^{q_1}} &= ax_1 - bx_1 y_1 + ex_1^2 - sz_1 x_1^2, \\ \frac{d^{q_2} y_1}{dt^{q_2}} &= dx_1 y_1 - cy_1, \\ \frac{d^{q_3} z_1}{dt^{q_3}} &= sz_1 x_1^2 - pz_1. \end{aligned} \quad (4)$$

The slave system with controllers is described by

$$\begin{aligned} \frac{d^{q_1} x_2}{dt^{q_1}} &= \alpha(y_2 - x_2) + u_1(t), \\ \frac{d^{q_2} y_2}{dt^{q_2}} &= \gamma y_2 - x_2 z_2 + u_2(t), \\ \frac{d^{q_3} z_2}{dt^{q_3}} &= x_2 y_2 - \beta z_2 + u_3(t), \end{aligned} \quad (5)$$

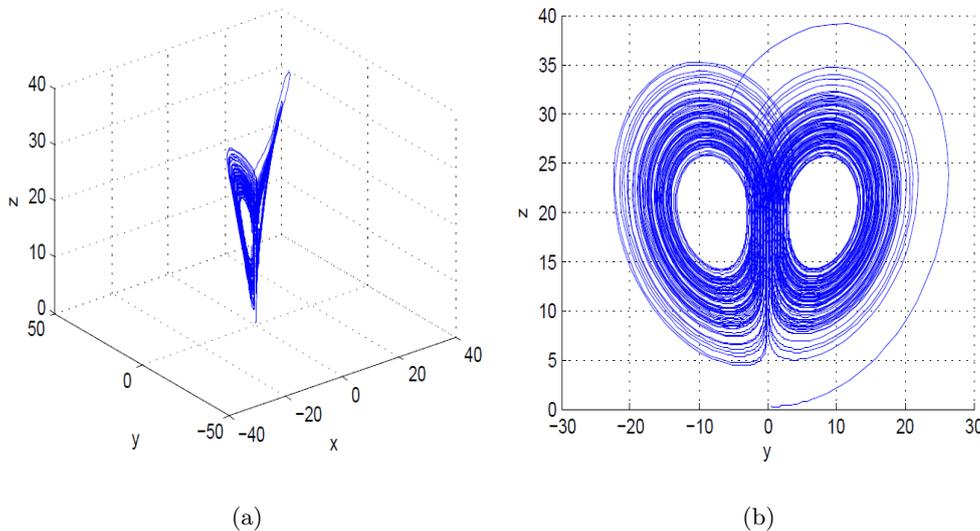


Figure 2: (a) Chaotic attractor of Lu system in $x - y - z$ space for $\alpha = 0.95$. (b) $y - z$ view of the Lu system for order $\alpha = 0.95$.

where $u_1(t), u_2(t), u_3(t)$ are three control functions. For complete synchronization, the error dynamical system is

$$\begin{aligned} \frac{d^{q_1} e_1}{dt^{q_1}} &= \alpha(e_2 - e_1) - (\alpha + a)x_1 + \alpha y_1 + bx_1 y_1 - ex_1^2 + sz_1 x_1^2 + u_1(t), \\ \frac{d^{q_2} e_2}{dt^{q_2}} &= \gamma e_2 - dx_1 y_1 + (\gamma + c)y_1 - x_2 z_2 + u_2(t), \\ \frac{d^{q_3} e_3}{dt^{q_3}} &= -\beta e_3 + x_2 y_2 - sz_1 x_1^2 + (p - \beta)z_1 + u_3(t). \end{aligned} \tag{6}$$

Define the active control functions $u_1(t), u_2(t), u_3(t)$ as

$$\begin{aligned} u_1(t) &= (\alpha + a)x_1 - \alpha y_1 - bx_1 y_1 + ex_1^2 - sz_1 x_1^2 + v_1(t), \\ u_2(t) &= dx_1 y_1 - (\gamma + c)y_1 + x_2 z_2 + v_2(t), \\ u_3(t) &= -x_2 y_2 + sz_1 x_1^2 - (p - \beta)z_1 + v_3(t). \end{aligned} \tag{7}$$

With these controllers the error dynamical system becomes

$$\begin{aligned} \frac{d^{q_1} e_1}{dt^{q_1}} &= \alpha(e_2 - e_1) + v_1(t), \\ \frac{d^{q_2} e_2}{dt^{q_2}} &= \gamma e_2 + v_2(t), \\ \frac{d^{q_3} e_3}{dt^{q_3}} &= -\beta e_3 + v_3(t). \end{aligned} \tag{8}$$

Define the suitable control inputs $v_1(t), v_2(t), v_3(t)$ to obtain the stable error dynamical system. Choosing $v_1(t), v_2(t), v_3(t)$ as

$$\begin{pmatrix} v_1(t) \\ v_2(t) \\ v_3(t) \end{pmatrix} = C \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix}, \tag{9}$$

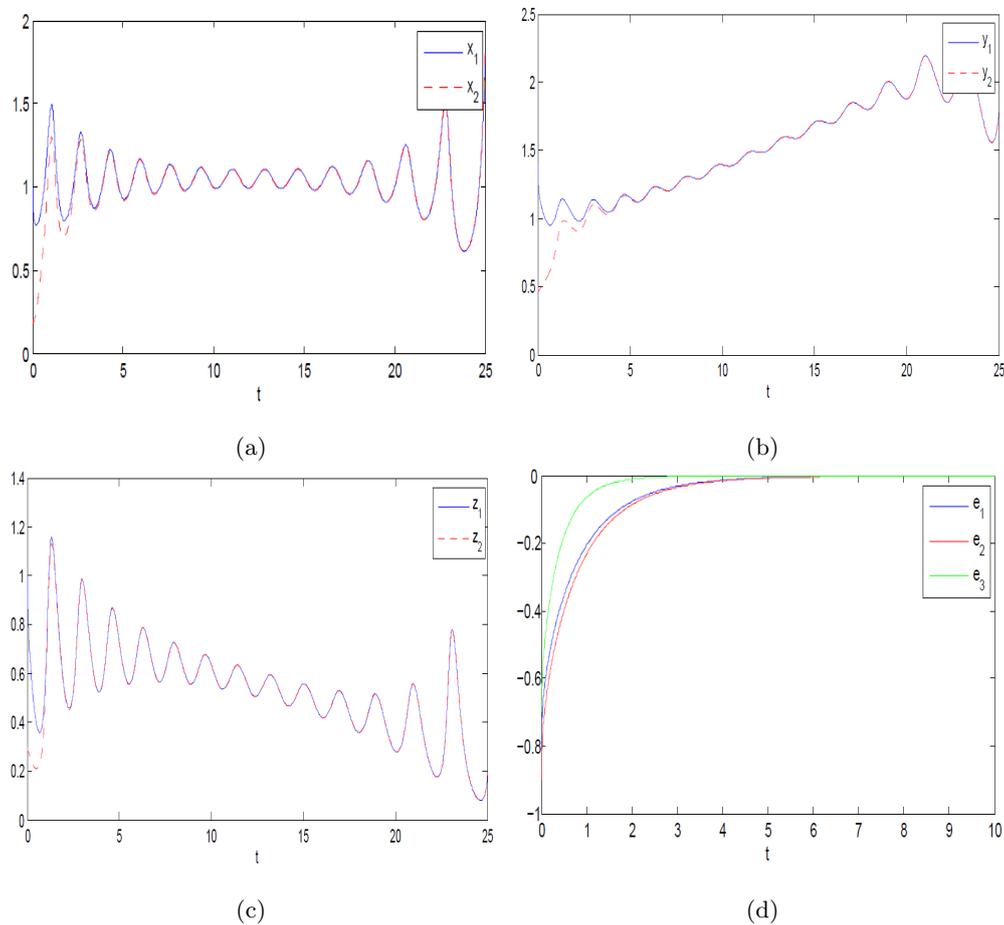


Figure 3: (a) Complete synchronization between state variables x_1, x_2 . (b) Complete synchronization between state variables y_1, y_2 . (c) Complete synchronization between state variables z_1, z_2 . (d) Complete synchronization errors e_1, e_2, e_3 converging to zero.

where C is a 3×3 constant matrix, we choose C as

$$\begin{pmatrix} (\alpha - 1) & -\alpha & 0 \\ 0 & -(\gamma + 1) & 0 \\ 0 & 0 & 1 \end{pmatrix}.$$

Then the error dynamical system is

$$\begin{aligned} \frac{d^{q_1} e_1}{dt^{q_1}} &= -e_1, \\ \frac{d^{q_2} e_2}{dt^{q_2}} &= -e_2, \\ \frac{d^{q_3} e_3}{dt^{q_3}} &= -2e_3. \end{aligned} \tag{10}$$

Eigenvalues for this error dynamical system are $-1, -1, -2$ which satisfies stability condition. Figures 3(a),(b),(c) show complete synchronization between state variables of master system and slave system, and 3(d) shows errors of complete synchronization converging to zero at the initial conditions $(-0.8, -0.9, -0.7)$. For anti-synchronization, we choose $\chi = -1$, and the error dynamical system for the same master and slave systems becomes

$$\begin{aligned} \frac{d^{q_1} e_1}{dt^{q_1}} &= \alpha(e_2 - e_1) + (\alpha + a)x_1 - \alpha y_1 - bx_1 y_1 + ex_1^2 - sz_1 x_1^2 + u_1(t), \\ \frac{d^{q_2} e_2}{dt^{q_2}} &= \gamma e_2 + dx_1 y_1 - (\gamma + c)y_1 - x_2 z_2 + u_2(t), \\ \frac{d^{q_3} e_3}{dt^{q_3}} &= -\beta e_3 + x_2 y_2 + sz_1 x_1^2 - (p - \beta)z_1 + u_3(t). \end{aligned} \tag{11}$$

The active control functions $u_1(t), u_2(t), u_3(t)$ are defined as

$$\begin{aligned} u_1(t) &= -(\alpha + a)x_1 + \alpha y_1 + bx_1 y_1 - ex_1^2 + sz_1 x_1^2 + v_1(t), \\ u_2(t) &= -dx_1 y_1 + (\gamma + c)y_1 + x_2 z_2 + v_2(t), \\ u_3(t) &= -x_2 y_2 - sz_1 x_1^2 + (p - \beta)z_1 + v_3(t), \end{aligned} \tag{12}$$

the error dynamical system becomes

$$\begin{aligned} \frac{d^{q_1} e_1}{dt^{q_1}} &= \alpha(e_2 - e_1) + v_1(t), \\ \frac{d^{q_2} e_2}{dt^{q_2}} &= \gamma e_2 + v_2(t), \\ \frac{d^{q_3} e_3}{dt^{q_3}} &= -\beta e_3 + v_3(t). \end{aligned} \tag{13}$$

Now we have to choose suitable control inputs $v_1(t), v_2(t), v_3(t)$ so that the stable error dynamical system could be obtained. Choosing $v_1(t), v_2(t), v_3(t)$ as

$$\begin{pmatrix} v_1(t) \\ v_2(t) \\ v_3(t) \end{pmatrix} = C \begin{pmatrix} e_1(t) \\ e_2(t) \\ e_3(t) \end{pmatrix}, \tag{14}$$

where C is a constant matrix and C is

$$\begin{pmatrix} (\alpha - 1) & -\alpha & 0 \\ 0 & -(\gamma + 1) & 0 \\ 0 & 0 & (\beta - 1) \end{pmatrix}.$$

Then the error dynamical system becomes

$$\begin{aligned} \frac{d^{q_1} e_1}{dt^{q_1}} &= -e_1, \\ \frac{d^{q_2} e_2}{dt^{q_2}} &= -e_2, \\ \frac{d^{q_3} e_3}{dt^{q_3}} &= -e_3. \end{aligned} \tag{15}$$

Eigenvalues for this error dynamical system are $-1, -1, -1$ which satisfies stability condition and initial conditions are $(1.2, 1.9, 1.3)$.

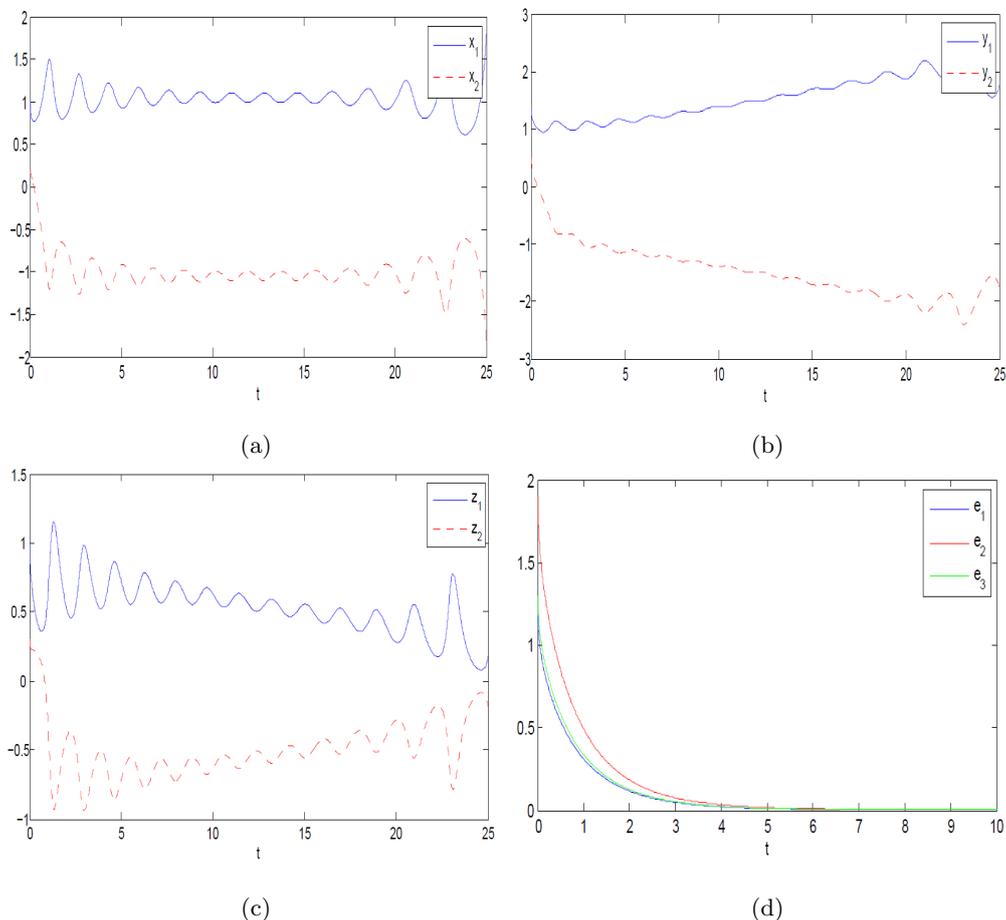


Figure 4: (a) Anti-synchronization between state variables x_1, x_2 . (b) Anti-synchronization between state variables y_1, y_2 . (c) Anti-synchronization between state variables z_1, z_2 . (d) Anti-synchronization errors e_1, e_2, e_3 converging to zero.

Figure 4(a),(b) shows anti-synchronization between state variables x_1, x_2 and y_1, y_2 , and Figure 4(c),(d) exhibits anti-synchronization between state variables z_1, z_2 and anti-synchronization errors tending to zero.

For projective synchronization the choice of the scalar χ is arbitrary, but we choose $\chi = 2$ and the error dynamical system with the same master and slave system becomes

$$\begin{aligned}
 \frac{d^{q_1} e_1}{dt^{q_1}} &= \alpha(e_2 - e_1) - 2(\alpha + a)x_1 + 2\alpha y_1 + 2bx_1 y_1 - 2ex_1^2 + 2sz_1 x_1^2 + u_1(t), \\
 \frac{d^{q_2} e_2}{dt^{q_2}} &= \gamma e_2 - 2dx_1 y_1 + 2(\gamma + c)y_1 - x_2 z_2 + u_2(t), \\
 \frac{d^{q_3} e_3}{dt^{q_3}} &= -\beta e_3 + x_2 y_2 - 2sz_1 x_1^2 + u_3(t).
 \end{aligned} \tag{16}$$

The active control functions $u_1(t), u_2(t), u_3(t)$ are defined as

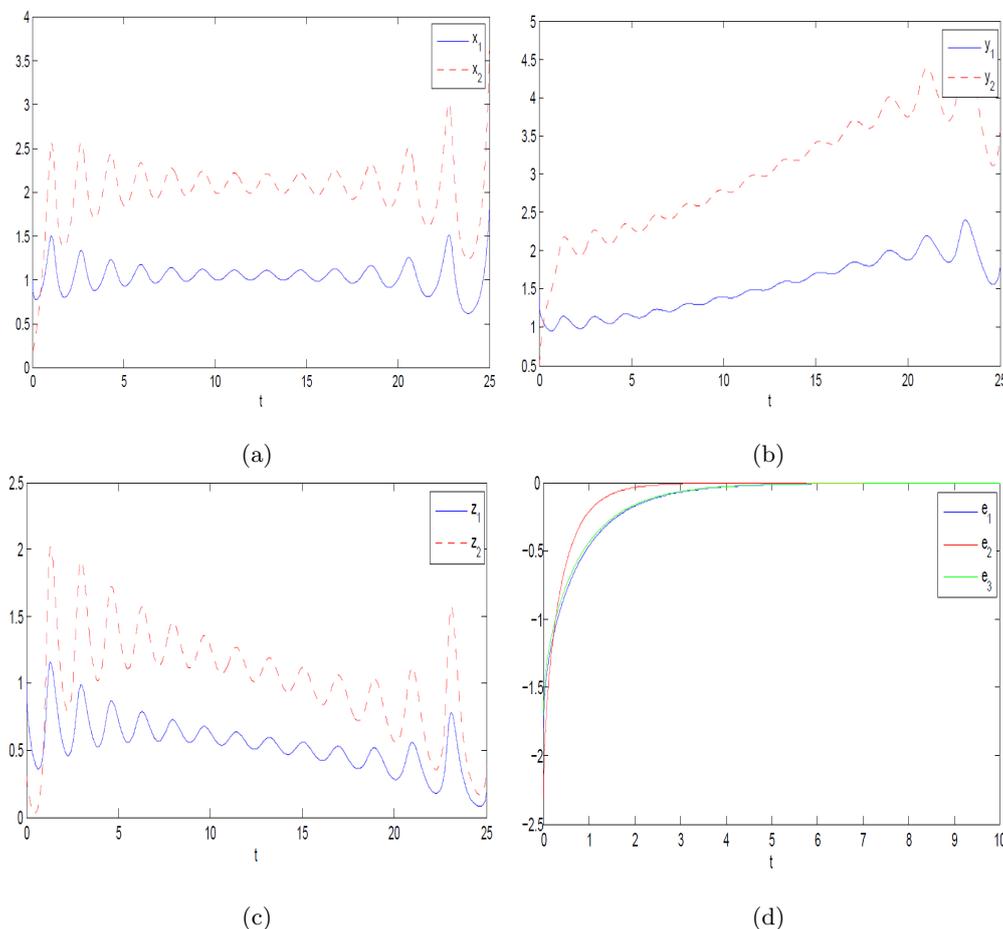


Figure 5: (a) Projective synchronization for state variables x_1, x_2 . (b) Projective synchronization for state variables y_1, y_2 . (c) Projective synchronization for state variables z_1, z_2 . (d) Projective synchronization errors e_1, e_2, e_3 converging to zero.

$$\begin{aligned}
 u_1(t) &= 2(\alpha + a)x_1 - 2\alpha y_1 - 2bx_1y_1 + 2ex_1^2 - 2sz_1x_1^2 + v_1(t), \\
 u_2(t) &= 2dx_1y_1 - 2(\gamma + c)y_1 + x_2z_2 + v_2(t), \\
 u_3(t) &= -x_2y_2 + 2sz_1x_1^2 + v_3(t).
 \end{aligned}
 \tag{17}$$

Then the error dynamical system becomes

$$\begin{aligned}
 \frac{d^{q_1}e_1}{dt^{q_1}} &= \alpha(e_2 - e_1) + v_1(t), \\
 \frac{d^{q_2}e_2}{dt^{q_2}} &= \gamma e_2 + v_2(t), \\
 \frac{d^{q_3}e_3}{dt^{q_3}} &= -\beta e_3 + v_3(t).
 \end{aligned}
 \tag{18}$$

Now we have to choose suitable control inputs $v_1(t), v_2(t), v_3(t)$ so that the stable error

dynamical system could be obtained. We choose $v_1(t), v_2(t), v_3(t)$ as follows

$$\begin{pmatrix} v_1(t) \\ v_2(t) \\ v_3(t) \end{pmatrix} = C \begin{pmatrix} e_1 \\ e_2 \\ e_3 \end{pmatrix}, \quad (19)$$

where C is a 3×3 constant matrix

$$\begin{pmatrix} (\alpha - 1) & -\alpha & 0 \\ 0 & -(\gamma + 2) & 0 \\ 0 & 0 & 2 \end{pmatrix}.$$

Then the error dynamical system becomes

$$\begin{aligned} \frac{d^{q_1} e_1}{dt^{q_1}} &= -e_1, \\ \frac{d^{q_2} e_2}{dt^{q_2}} &= -2e_2, \\ \frac{d^{q_3} e_3}{dt^{q_3}} &= -e_3. \end{aligned} \quad (20)$$

Eigenvalues for this error dynamical system are $-1, -2, -1$ which satisfies stability condition and initial conditions for this error dynamical system are $(-1.8, -2.3, -1.7)$. Figure 5 (a),(b),(c) shows projective synchronization between state variables of master system and slave system and Figure 5(d) exhibits projective synchronization errors converging to zero .

5 Conclusion

Different types of synchronizations have been achieved between two different fractional order chaotic systems Lotka-Volterra system and Lu system by using active control method. The method is easy to apply. The results are validated by numerical simulations using Matlab. Numerical simulations are a witness to achievement of desired goal between these two systems. The analytical and computational results are in an excellent agreement.

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